



# What is *VOACAP* Trying to Tell Me?

A Presentation to  
The Yankee Clipper Contest Club

Feb. 1, 2003  
Milford, CT

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Senior Assistant Technical Editor, ARRL



## *VOACAP*

- *VOACAP* has been under development by the US government for more than three solar cycles.
- *VOACAP* is recognized as being an accurate propagation-prediction program.
- *VOACAP* produces *reams* of output data and forces the user to make information from it!

**There is a big difference between *data* and *information*.**



## *VOACAP*

You must give *VOACAP* a number of parameters before it can do a propagation prediction.

The most important selections are the **Method** and the **Antennas** used.



# VOACAP Inputs

Method

Month, SSN

Tx & Rx QTHs

Freq.

System

Tx & Rx Antennas

VOACAP Point-to-Point data input

File Run View Save to: Help

|             |   |                          |
|-------------|---|--------------------------|
| Method      | 25 = All modes table  |                          |
| Year        | 1994  | Coefficients CCIR (Oslo) |
| Time        | 01 to 24 by 1 hours UT  |                          |
| Groups      | Month.Day= 11.00<br>SSN = 120   |                          |
| Transmitter | 42.37N 71.05W BOSTON  |                          |
| Receiver    | 51.50N 0.17W LONDON   |                          |
| Path        | Short Distances: 5260km 2840nmi 3268mi Azimuth: 53.2deg   |                          |
| Freq(MHz)   | 28.400  |                          |
| System      | Noise Level 4 Min Angle 0.10deg Req.Rel. 50% Req SNR 43dB Multi Tol 3.00dB Multi Del 0.10msec                               |                          |
| Eprob       | 1.00*foE 1.00*foF1 1.00*foF2 0.00*foEs  |                          |
| Ix Antenna  | # Min Max Design Directory\Filename.sfx Model MainBeam Power kW<br>1 2 30 10.888 samples \SAMPLE.00 + 10.0 dBi 53.2 15.0000 |                          |
| Rx Antenna  | Samples \SAMPLE.00 293.1deg 10.00dB   |                          |

Input Help:



# *VOACAP* Methods

- There are 30 “Methods” in *VOACAP*.
- Most are not useful to the contester.
- I use Method 25 (All Modes) and Method 30 (short-long path smoothing) most often.
- Method 30 gets rid of anomalies between 7,000 to 10,000 km (what *IONCAP* calls “short” and “long” paths).



# VOACAP Methods

Change propagation METHOD

Accept Cancel

Select the Propagation METHOD to use:

- 1 = Ionospheric parameters
- 2 = Ionograms
- 3 = MUF-FOT lines (nomogram)
- 4 = MUF-FOT graph (use 11 or 28)
- 5 = HPF-MUF-FOT graph
- 6 = MUF-FOT-Es graph (use 11)
- 7 = FOT-MUF table (full ionosphere)
- 8 = MUF-FOT graph (use 11 or 28)
- 9 = HPF-MUF-FOT graph
- 10 = MUF-FOT-ANG graph
- 11 = MUF-FOT-Es graph - real graph, not line printer
- 12 = MUF by magnetic indices, K(not implemented)
- 13 = Transmitter antenna pattern
- 14 = Receiver antenna pattern
- 15 = Both transmitter & receiver antenna patterns
- 16 = System performance (S.P.)
- 17 = Condensed system performance, reliability
- 18 = Condensed system performance, service probability
- 19 = Propagation path geometry
- 20 = Complete system performance (C.S.P.)
- 21 = Forced long path model (C.S.P.)
- 22 = Forced short path model (C.S.P.)
- 23 = User selected output (set by TOPLINES & BOTLINES)
- 24 = MUF-REL table
- 25 = All modes table**
- 26 = MUF-LUF-FOT table (nomogram)
- 27 = FOT-LUF graph (use 28)
- 28 = MUF-FOT-LUF graph - real graph, not line printer
- 29 = MUF-LUF graph (use 28)
- 30 = For VOACAP only - S/L path smoothing (7-10000 km)

All modes table

S/L path smoothing



# VOACAP Method 25 Output

CCIR Coefficients      ~METHOD 25      VOACAP 02.1106W      PAGE      2

Feb      2003      SSN =      90.      Minimum Angle= 0.100 degrees  
BOSTON      LONDON      AZIMUTHS      N. MI.      KM  
42.37 N      71.05 W - 51.50 N      0.17 W      53.15      288.25      2840.2      5259.6  
XMTR 2-30 + 10.0 dBi[samples\SAMPLE.00      ] Az= 53.2 OFFaz=360.0      15.000kW  
RCVR 2-30 + 10.0 dBi[samples\SAMPLE.00      ] Az=293.1 OFFaz=355.1  
3 MHz NOISE = -163.6 dBW      REQ. REL = 50%      REQ. SNR = 43.0 dB

SUMMARY      3 MODES      FREQ =      7.2 MHZ      UT =      1.0  
Most REL

|           |         |            |         |        |     |     |
|-----------|---------|------------|---------|--------|-----|-----|
|           | 2.F2    | 3.F2       | 3. E    | 2.F2   |     |     |
| TIME DEL. | 18.41   | 19.17      | 17.88   | 18.41  |     |     |
| ANGLE     | 7.06    | 16.30      | 4.10    | 7.06   |     |     |
| VIR. HITE | 311.51  | 332.19     | 125.30  | 311.51 |     |     |
| TRAN.LOSS | 123.63  | 125.75     | 947.56  | 123.63 |     |     |
| T. GAIN   | 10.00   | 10.00      | 10.00   | 10.00  |     |     |
| R. GAIN   | 10.00   | 10.00      | 10.00   | 10.00  |     |     |
| ABSORB    | 4.09    | 2.66       | 4.62    |        |     |     |
| FS. LOSS  | 124.43  | 124.79     | 124.18  |        |     |     |
| FIELD ST. | 32.48   | 30.36      | -791.46 | 34.56  |     |     |
| SIG. POW. | -81.86  | -83.99     | -905.80 | -79.79 |     |     |
| SNR       | 76.25   | 74.13      | -747.69 | 78.33  |     |     |
| MODE PROB | 0.99    | 0.83       | 0.00    | 0.99   |     |     |
| R. PWRG   | 1000.00 | 1000.00    | 1000.00 | -35.33 |     |     |
| RELIABIL  | 1.00    | 0.99       | 0.00    | 1.00   |     |     |
| SERV PROB | 1.00    | 1.00       | 0.00    | 1.00   |     |     |
| SIG LOW   | 9.09    | 15.16      | 8.61    | 10.55  |     |     |
| SIG UP    | 4.88    | 5.39       | 4.86    | 5.08   |     |     |
| NOISE =   | -158    | S. POWER = | -79.8   |        |     |     |
| SIGNAL =  | 8.6     | 10.1       | 4.9 /   | 1.8    | 5.7 | 1.0 |
| NOISE =   | 6.2     | -158.1     | 5.1 /   | 2.2    | 3.3 | 2.0 |
| RELIAB =  | 7.2     | 78.3       | 12.2    |        |     |     |
| SPROB =   | 6.8     | 76.2       | 6.8     |        |     |     |



Mode



Elev. angle



Signal power, dBW



SNR, in 1 Hz BW



Mode probability

**All modes for one  
frequency, for each  
hour -- the output  
file is huge!**



# Sample *VOACAP* Method 25 Output

CCIR Coefficients      ~METHOD 25    VOACAP 02.1106W    PAGE    2

Feb    2003                    SSN =    90.                    Minimum Angle= 0.100 degrees  
BOSTON                    LONDON                    AZIMUTHS                    N. MI.                    KM  
42.37 N    71.05 W - 51.50 N    0.17 W                    53.15    288.25                    2840.2                    5259.6  
XMTR 2-30 + 10.0 dBi[samples\SAMPLE.00    ] Az= 53.2 OFFaz=360.0    15.000kW  
RCVR 2-30 + 10.0 dBi[samples\SAMPLE.00    ] Az=293.1 OFFaz=355.1  
3 MHz NOISE = -163.6 dBW                    REQ. REL = 50%                    REQ. SNR = 43.0 dB

SUMMARY    3 MODES    FREQ =    7.2 MHZ    UT =    1.0  
Most REL

|            |         |            |           |            |
|------------|---------|------------|-----------|------------|
|            | 2.F2    | 3.F2       | 3. E      | 2.F2       |
| TIME DEL.  | 18.41   | 19.17      | 17.88     | 18.41      |
| ANGLE      | 7.06    | 16.30      | 4.10      | 7.06       |
| VIR. HITE  | 311.51  | 332.19     | 125.30    | 311.51     |
| TRAN. LOSS | 123.63  | 125.75     | 947.56    | 123.63     |
| T. GAIN    | 10.00   | 10.00      | 10.00     | 10.00      |
| R. GAIN    | 10.00   | 10.00      | 10.00     | 10.00      |
| ABSORB     | 4.09    | 2.66       | 4.62      |            |
| FS. LOSS   | 124.43  | 124.79     | 124.18    |            |
| FIELD ST.  | 32.48   | 30.36      | -791.46   | 34.56      |
| SIG. POW.  | -81.86  | -83.99     | -905.80   | -79.79     |
| SNR        | 76.25   | 74.13      | -747.69   | 78.33      |
| MODE PROB  | 0.99    | 0.83       | 0.00      | 0.99       |
| R. PWRG    | 1000.00 | 1000.00    | 1000.00   | -35.33     |
| RELIABIL   | 1.00    | 0.99       | 0.00      | 1.00       |
| SERV PROB  | 1.00    | 1.00       | 0.00      | 1.00       |
| SIG LOW    | 9.09    | 15.16      | 8.61      | 10.55      |
| SIG UP     | 4.88    | 5.39       | 4.86      | 5.08       |
| NOISE =    | -158    | S. POWER = | -79.8     |            |
| SIGNAL =   | 8.6     | 10.1       | 4.9 / 1.8 | 5.7    1.0 |
| NOISE =    | 6.2     | -158.1     | 5.1 / 2.2 | 3.3    2.0 |
| RELIAB =   | 7.2     | 78.3       | 12.2      |            |
| SPROB =    | 6.8     | 76.2       | 6.8       |            |

**Two 7.2-MHz modes:  
2.F2 at 7.06° and 3.F2 at  
16.30° takeoff angles.**

**The signal power at the  
receiver is -81.86 dBW  
and -83.99 dBW -- very  
close, so fading can easily  
occur.**





## Sample *VOACAP* Method 25 Output

Let's drill down and look more closely at the information around 1200 UTC, East-Coast sunrise on 15 meters.

Here's how to convert from dBW to dB $\mu$ V:

$$\text{dB}\mu\text{V} = 137 + \text{dBW}$$

$$\text{Now, } 34 \text{ dB}\mu\text{V} = \text{S9}$$

$$\text{So, } -103 \text{ dBW} = \text{S9, and } -93 \text{ dBW} = \text{S9+10.}$$



# Edited *VOACAP* Method 25 Output

Elevation Angle

|           |        |         |        |
|-----------|--------|---------|--------|
| UT = 12.0 | 2.F2   | 2.F2    | 2.F2   |
| ANGLE     | 7.04   | 10.25   | 7.04   |
| SIG. POW. | -98.66 | -112.02 | -98.46 |
| SNR       | 82.59  | 69.22   | 82.78  |
| MODE PROB | 0.56   | 0.56    | 0.56   |

S9+4

S7, Pedersen  
wave

VOACAP's  
choice of Most  
Reliable Mode  
(MRM) = 56% of  
days in the month



# Edited *VOACAP* Method 25 Output

|           |        |         |         |         |   |                                   |
|-----------|--------|---------|---------|---------|---|-----------------------------------|
| UT = 12.0 | 2.F2   | 2.F2    | 2.F2    |         |   |                                   |
| ANGLE     | 7.04   | 10.25   | 7.04    |         |   |                                   |
| SIG. POW. | -98.66 | -112.02 | -98.46  | ←       | 12 UTC: Pedersen wave on 2.F2 is weaker |                                   |
| SNR       | 82.59  | 69.22   | 82.78   |         |   |                                   |
| MODE PROB | 0.56   | 0.56    | 0.56    |         |   |                                   |
| UT = 13.0 | 2.F2   | 2.F2    |         |         |   |                                   |
| ANGLE     | 4.64   | 4.64    |         | ←       | 13 UTC: 1 mode only, no Pedersen        |                                   |
| SIG. POW. | -92.39 | -92.39  |         |         |   |                                   |
| SNR       | 87.95  | 87.95   |         |         |   |                                   |
| MODE PROB | 0.89   | 0.89    |         |         |   |                                   |
| UT = 14.0 | 2.F2   | 3.F2    | 3.F2    | 3.E     | 2.F2                                    |                                   |
| ANGLE     | 4.40   | 13.89   | 17.01   | 4.10    | 4.40                                    | ←                                 |
| SIG. POW. | -93.26 | -102.87 | -113.59 | -686.02 | -92.77                                  | 14 UTC: 3 modes; Pedersen on 3.F2 |
| SNR       | 85.94  | 76.33   | 65.60   | -506.82 | 86.42                                   |                                   |
| MODE PROB | 0.92   | 0.41    | 0.41    | 0.00    | 0.92                                    |                                   |
| UT = 15.0 | 2.F2   | 3.F2    | 3.F2    | 3.E     | 2.F2                                    |                                   |
| ANGLE     | 4.78   | 14.03   | 18.30   | 4.10    | 4.78                                    | ←                                 |
| SIG. POW. | -93.70 | -101.82 | -118.36 | -857.80 | -93.07                                  | 15 UTC: 3 modes; Pedersen on 3.F2 |
| SNR       | 85.58  | 77.46   | 60.92   | -678.52 | 86.21                                   |                                   |
| MODE PROB | 0.93   | 0.47    | 0.47    | 0.00    | 0.93                                    |                                   |
| UT = 16.0 | 2.F2   | 3.F2    | 3.F2    | 3.E     | 2.F2                                    |                                   |
| ANGLE     | 4.86   | 14.68   | 18.16   | 4.10    | 4.86                                    | ←                                 |
| SIG. POW. | -92.68 | -102.42 | -116.01 | -919.18 | -92.22                                  | 16 UTC: 3 modes; Pedersen on 3.F2 |
| SNR       | 86.71  | 76.96   | 63.37   | -739.80 | 87.17                                   |                                   |
| MODE PROB | 0.93   | 0.44    | 0.44    | 0.00    | 0.93                                    |                                   |
| UT = 17.0 | 2.F2   | 2.F2    |         |         |   |                                   |
| ANGLE     | 5.02   | 5.02    |         |         |   |                                   |
| SIG. POW. | -90.60 | -90.60  |         |         |   | ←                                 |
| SNR       | 88.90  | 88.90   |         |         |   | 17 UTC: 1 mode only, no Pedersen  |
| MODE PROB | 0.94   | 0.94    |         |         |   |                                   |



# *VOACAP* Antenna Selection

- To see a propagation prediction without bias due to antenna type or height, I usually choose “isotropic” Tx and Rx antennas, but with +10 dBi gain to simulate real-world gains.
- The resulting gain shows in the TGAIN and RGAIN lines in the output printout.



# VOACAP Method 30 Output

Feb 2003 SSN = 90. Minimum Angle= 0.100 degrees  
BOSTON LONDON AZIMUTHS N. MI. KM  
42.37 N 71.05 W - 51.50 N 0.17 W 53.15 288.25 2840.2 5259.6  
XMTR 2-30 + 10.0 dBi[samples\SAMPLE.00 ] Az= 53.2 OFFaz=360.0 15.000kW  
RCVR 2-30 + 10.0 dBi[samples\SAMPLE.00 ] Az=293.1 OFFaz=355.1  
3 MHz NOISE = -163.6 dBW REQ. REL = 50% REQ. SNR = 43.0 dB  
MULTIPATH POWER TOLERANCE = 3.0 dB MULTIPATH DELAY TOLERANCE = 0.100 ms

|      |      |      |      |      |      |      |      |     |     |     |     |     |       |        |   |
|------|------|------|------|------|------|------|------|-----|-----|-----|-----|-----|-------|--------|---|
| MUF  | 1.0  | 10.5 | 3.6  | 7.2  | 14.1 | 21.2 | 28.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0   | FREQ   |   |
|      | 2F2  | 2F2  | 2F2  | 2F2  | 2F2  | 2F2  | 2F2  | -   | -   | -   | -   | -   | -     | MODE   | ← |
|      | 12.4 | 6.8  | 7.1  | 12.4 | 12.4 | 12.4 | 12.4 | -   | -   | -   | -   | -   | -     | TANGLE | ← |
|      | 19.1 | 18.4 | 18.4 | 19.1 | 19.1 | 19.1 | 19.1 | -   | -   | -   | -   | -   | -     | DELAY  |   |
|      | 453  | 305  | 312  | 453  | 453  | 453  | 453  | -   | -   | -   | -   | -   | -     | V HITE |   |
|      | 0.50 | 1.00 | 0.99 | 0.07 | 0.00 | 0.00 | 0.00 | -   | -   | -   | -   | -   | -     | MUFday | ← |
|      | 139  | 129  | 124  | 184  | 364  | 409  | 409  | -   | -   | -   | -   | -   | -     | LOSS   |   |
|      | 20   | 24   | 35   | -22  | -199 | -241 | -241 | -   | -   | -   | -   | -   | -     | DBU    |   |
|      | -97  | -84  | -80  | -143 | -322 | -368 | -368 | -   | -   | -   | -   | -   | -     | S DBW  | ← |
|      | -167 | -148 | -158 | -176 | -183 | -186 | -186 | -   | -   | -   | -   | -   | -     | N DBW  |   |
|      | 70   | 63   | 78   | 34   | -139 | -182 | -182 | -   | -   | -   | -   | -   | -     | SNR    | ← |
|      | -27  | -20  | -35  | 9    | 182  | 225  | 225  | -   | -   | -   | -   | -   | -     | RPWRG  |   |
|      | 0.91 | 0.99 | 1.00 | 0.32 | 0.00 | 0.00 | 0.00 | -   | -   | -   | -   | -   | -     | REL    |   |
|      | 0.00 | 0.95 | 0.99 | 0.00 | 0.00 | 0.00 | 0.00 | -   | -   | -   | -   | -   | -     | MPROB  |   |
|      | 1.00 | 0.99 | 1.00 | 0.07 | 0.00 | 0.00 | 0.00 | -   | -   | -   | -   | -   | -     | S PRB  |   |
|      | 25.0 | 8.6  | 10.6 | 25.0 | 25.0 | 8.6  | 8.6  | -   | -   | -   | -   | -   | -     | SIG LW |   |
|      | 20.8 | 4.9  | 5.1  | 25.0 | 25.0 | 4.9  | 4.9  | -   | -   | -   | -   | -   | -     | SIG UP |   |
|      | 25.5 | 11.9 | 12.2 | 25.9 | 26.1 | 11.3 | 11.3 | -   | -   | -   | -   | -   | -     | SNR LW |   |
|      | 21.1 | 8.2  | 7.2  | 25.1 | 25.1 | 5.5  | 5.5  | -   | -   | -   | -   | -   | -     | SNR UP |   |
|      | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | -   | -   | -   | -   | -   | -     | TGAIN  | ← |
| 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | -    | -   | -   | -   | -   | -   | RGAIN | ←      |   |
| 70   | 63   | 78   | 34   | -139 | -182 | -182 | -    | -   | -   | -   | -   | -   | SNRxx |        |   |

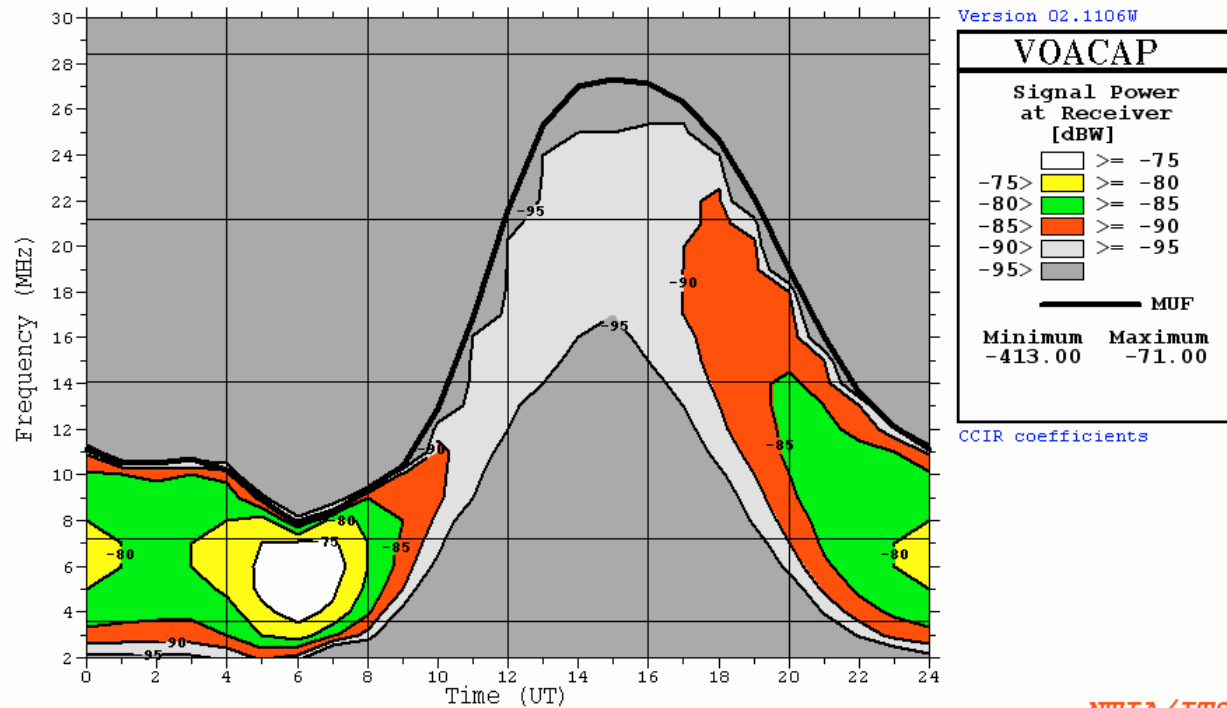
**Summary of all frequencies for each hour**



# VOACAP Graph Output

SDBW = -93.00 at UT=14.07(14:04) Freq= 21.177 MHz

```
Feb 2003          SSN = 90.          Minimum Angle= 0.100 degrees
BOSTON           LONDON              AZIMUTHS          N. MI.          KM
42.37 N  71.05 W - 51.50 N  0.17 W   53.15  288.25   2840.2   5259.6
XMTR 2-30 + 10.0 dBi[samples\SAMPLE.00 ] Az= 53.2 OFFaz=360.0  15.000kW
RCVR 2-30 + 10.0 dBi[samples\SAMPLE.00 ] Az=293.1 OFFaz=355.1
3 MHz NOISE = -163.6 dBW   REQ. REL = 50%   REQ. SNR = 43.0 dB
MULTIPATH POWER TOLERANCE = 3.0 dB   MULTIPATH DELAY TOLERANCE = 0.100 ms
```



**This looks pretty, but it doesn't really give that much useful information for contest planning!**



# *VOACAP* Output Information

**I use two types of information from  
*CAPMAN/VOACAP*:**

- Elevation angle statistics
- Signal-strength predictions



# Elevation-Angle Statistics

- About ten years ago I started a detailed study at ARRL HQ on the range of elevation angles needed for communication between various QTHs around the world.
- I used the *VOACAP* program, along with some proprietary software, to create some *huge* databases. From these, elevation I generated statistics for 150+ QTHs around the world.





# Elevation-Angle Statistics

A tiny portion of the raw database from Boston to the world.

| RxQTH  | Freq | SSN | Month | Hour | dBuV | Elev | Rel   | Mode |
|--------|------|-----|-------|------|------|------|-------|------|
| London | 3.6  | 5   | 2     | 0    | 38.5 | 5.6  | 0.690 | 2.F2 |
| London | 3.6  | 5   | 2     | 0    | 35.9 | 13.0 | 0.580 | 3.F2 |
| London | 3.6  | 5   | 2     | 0    | 33.6 | 19.4 | 0.490 | 4.F2 |
| London | 3.6  | 5   | 2     | 1    | 38.9 | 5.6  | 0.660 | 2.F2 |
| London | 3.6  | 5   | 2     | 1    | 36.4 | 13.1 | 0.570 | 3.F2 |
| London | 3.6  | 5   | 2     | 1    | 34.3 | 19.6 | 0.500 | 4.F2 |
| London | 3.6  | 5   | 2     | 2    | 38.3 | 5.5  | 0.620 | 2.F2 |
| London | 3.6  | 5   | 2     | 2    | 35.7 | 13.0 | 0.530 | 3.F2 |
| London | 3.6  | 5   | 2     | 2    | 33.7 | 19.5 | 0.420 | 4.F2 |
| London | 3.6  | 5   | 2     | 3    | 37.9 | 5.5  | 0.640 | 2.F2 |
| London | 3.6  | 5   | 2     | 3    | 35.3 | 13.0 | 0.550 | 3.F2 |
| London | 3.6  | 5   | 2     | 3    | 33.3 | 19.4 | 0.470 | 4.F2 |
| London | 3.6  | 5   | 2     | 4    | 39.6 | 5.6  | 0.710 | 2.F2 |
| London | 3.6  | 5   | 2     | 4    | 37.1 | 13.2 | 0.630 | 3.F2 |



## Elevation-Angle Statistics

- The resulting elevation-angle files are on the CD-ROM in *The ARRL Antenna Book*. They contain statistical averages over the entire 11-year solar cycle -- for all months of the year and for all hours of the day.
- These statistical files are used by the *YT* and *HFTA* terrain-assessment programs.



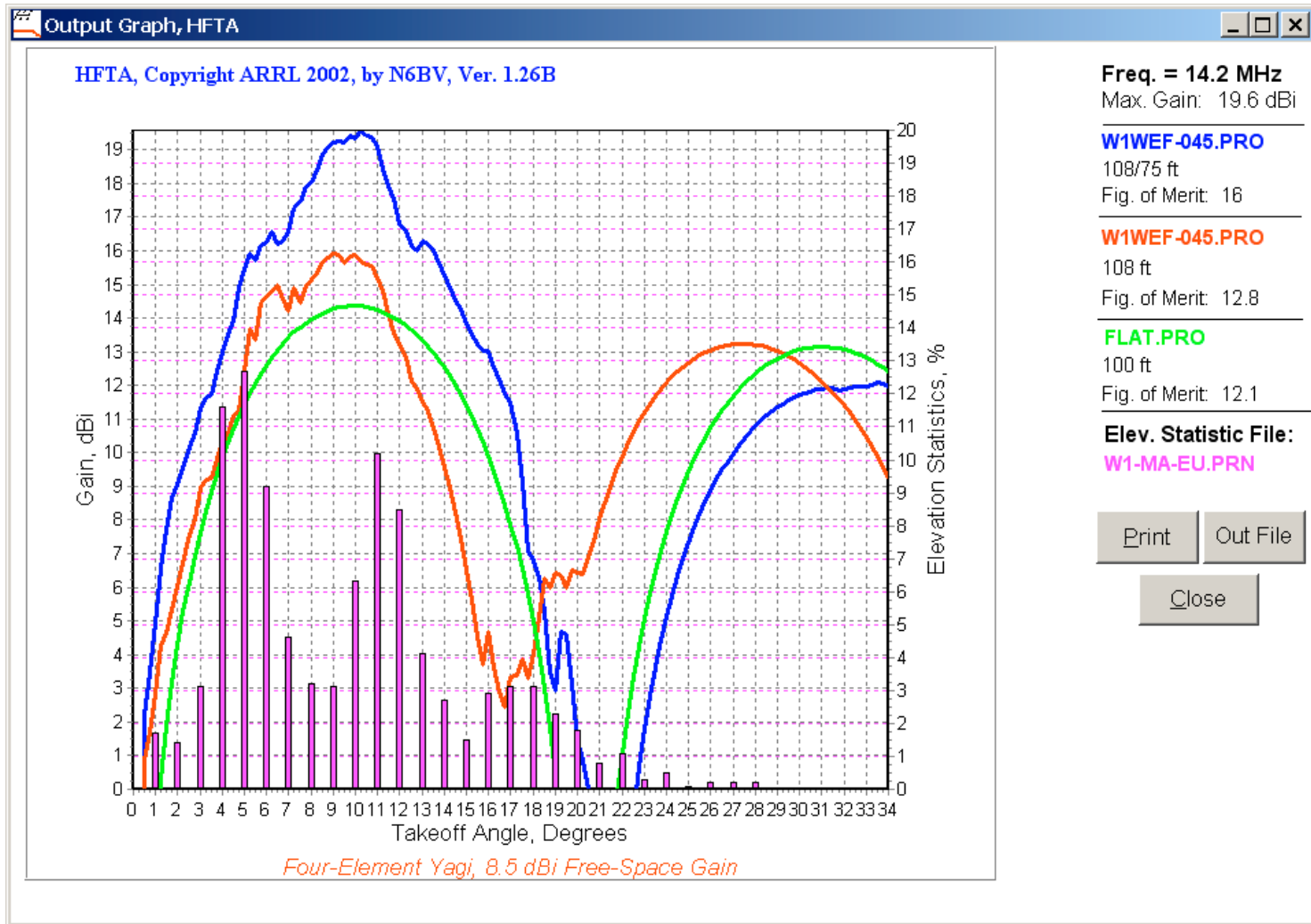
# Sample Table, Boston to Europe

Boston, Massachusetts to Europe

| Elev | 80m  | 40m | 30m | 20m  | 17m  | 15m  | 12m  | 10m  |
|------|------|-----|-----|------|------|------|------|------|
| 1    | 4.1  | 9.6 | 4.6 | 1.7  | 2.1  | 4.4  | 5.5  | 7.2  |
| 2    | 0.8  | 2.3 | 7.2 | 1.4  | 2.8  | 2.8  | 3.7  | 5.3  |
| 3    | 0.3  | 0.7 | 4.3 | 3.1  | 2.4  | 2.2  | 4.4  | 7.9  |
| 4    | 0.5  | 4.1 | 8.7 | 11.6 | 12.2 | 9.4  | 8.1  | 3.9  |
| 5    | 4.6  | 4.8 | 7.5 | 12.7 | 14.3 | 13.1 | 9.2  | 11.2 |
| 6    | 7.1  | 8.9 | 5.5 | 9.2  | 9.6  | 12.2 | 9.2  | 7.2  |
| 7    | 8.5  | 6.9 | 7.2 | 4.6  | 7.9  | 7.4  | 10.0 | 5.9  |
| 8    | 5.1  | 7.0 | 5.4 | 3.2  | 5.9  | 7.4  | 4.8  | 6.6  |
| 9    | 3.3  | 5.6 | 3.2 | 3.1  | 2.1  | 3.9  | 8.1  | 9.2  |
| 10   | 1.0  | 4.0 | 7.9 | 6.3  | 5.1  | 3.7  | 11.1 | 6.6  |
| 11   | 1.9  | 3.8 | 9.7 | 10.2 | 7.2  | 5.4  | 3.7  | 7.9  |
| 12   | 5.6  | 3.4 | 4.8 | 8.5  | 6.9  | 7.4  | 4.8  | 6.6  |
| 13   | 11.0 | 3.0 | 2.4 | 4.1  | 5.9  | 4.6  | 3.3  | 2.6  |
| 14   | 7.6  | 4.8 | 2.0 | 2.7  | 3.8  | 3.9  | 6.3  | 5.9  |
| 15   | 5.3  | 7.9 | 2.0 | 1.5  | 2.4  | 1.7  | 1.5  | 2.0  |
| 16   | 2.8  | 6.4 | 3.8 | 2.9  | 1.5  | 1.3  | 2.6  | 2.6  |
| 17   | 5.0  | 3.4 | 4.5 | 3.1  | 1.0  | 1.5  | 0.0  | 0.0  |
| 18   | 4.2  | 2.0 | 3.1 | 3.1  | 2.0  | 2.2  | 1.8  | 1.3  |
| 19   | 5.7  | 1.4 | 1.4 | 2.3  | 1.3  | 0.7  | 0.0  | 0.0  |
| 20   | 6.6  | 1.4 | 1.2 | 1.8  | 1.1  | 1.3  | 0.7  | 0.0  |
| 21   | 4.4  | 1.4 | 0.5 | 0.8  | 0.7  | 0.7  | 0.4  | 0.0  |
| 22   | 2.3  | 2.4 | 1.0 | 1.1  | 0.6  | 1.3  | 0.7  | 0.0  |
| 23   | 1.3  | 1.8 | 0.1 | 0.3  | 0.1  | 0.0  | 0.0  | 0.0  |
| 24   | 0.6  | 1.0 | 0.5 | 0.5  | 0.4  | 0.7  | 0.0  | 0.0  |
| 25   | 0.3  | 0.8 | 0.3 | 0.1  | 0.4  | 0.0  | 0.0  | 0.0  |
| 26   | 0.0  | 0.5 | 0.7 | 0.2  | 0.1  | 0.4  | 0.0  | 0.0  |
| 27   | 0.1  | 0.1 | 0.1 | 0.2  | 0.1  | 0.2  | 0.0  | 0.0  |
| 28   | 0.0  | 0.3 | 0.1 | 0.2  | 0.0  | 0.2  | 0.0  | 0.0  |
| 29   | 0.1  | 0.0 | 0.2 | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |
| 30   | 0.0  | 0.1 | 0.0 | 0.0  | 0.0  | 0.0  | 0.0  | 0.0  |



# One Picture = 1000 Words





# Propagation Predictions

YCCC members are familiar with the predictions I provide for the major DX contests (CQWW Phone, CW and ARRL DX Phone, CW).

These show tables of predictions, one page per band. Each page shows predictions for 40 CQ Zones, for 24 hours.

These are computed for undisturbed ionospheric conditions.



# Sample Propagation Prediction

15 Meters: Feb. 2003, YCCC, for SSN = High, Sigs in S-Units. By N6BV, ARRL.

| Zone     | UTC --> |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |   |
|----------|---------|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|---|
|          | 00      | 01 | 02 | 03 | 04 | 05 | 06 | 07 | 08 | 09 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |   |
| KL7 = 01 | 9       | 5  | 1  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 2  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ |   |
| VO2 = 02 | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 5  | 7  | 8  | 8  | 8  | 7  | 4  | 1  | 4  |   |
| W6 = 03  | 9+      | 9  | 2  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 5  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |   |
| W0 = 04  | 9+      | 9+ | 6  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |   |
| W3 = 05  | 1       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 1  | 1  | 1  | 1  | 1  | -  | -  | -  | -  | -  | -  | 1  |   |
| XE1 = 06 | 9       | 5  | 9  | 7  | 1  | 1  | 1  | 2  | 5  | 4  | -  | -  | 8  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |   |
| TI = 07  | 9       | 4  | 9  | 7  | 5  | 3  | 2  | 3  | 4  | 2  | -  | 2  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |   |
| VP2 = 08 | 9+      | 9  | 7  | 4  | 4  | 4  | 4  | 4  | 1  | -  | 4  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |   |
| P4 = 09  | 9       | 9+ | 8  | 7  | 6  | 6  | 5  | 6  | 3  | -  | 1  | 4  | 8  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |   |
| HC = 10  | 8       | 7  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 7  | 5  | 9+ | 9+ | 9+ | 9  | 9  | 9  | 9  | 9+ | 9+ | 4  |   |
| PY1 = 11 | 9       | 7  | 4  | 2  | 3  | 4  | 4  | 1  | -  | -  | 2  | 9  | 9+ | 9  | 8  | 7  | 8  | 8  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ |   |
| CE = 12  | 9+      | 8  | 5  | 4  | 3  | 3  | 2  | 2  | -  | -  | -  | 9  | 9  | 8  | 8  | 7  | 8  | 8  | 9  | 9  | 9  | 9+ | 9+ | 9+ |   |
| LU = 13  | 9+      | 7  | 5  | 4  | 2  | 4  | 4  | 3  | -  | -  | 5  | 9+ | 9  | 8  | 7  | 7  | 8  | 8  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ |   |
| G = 14   | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 2  | -  | -  | -  |   |
| I = 15   | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 6  | 9+ | 9+ | 9+ | 9+ | 9+ | 8  | 9  | 2  | -  | -  | -  | -  |   |
| UA3 = 16 | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 6  | 9  | 9  | 9  | 8  | 5  | 1  | -  | -  | -  | -  | -  | -  |   |
| UN = 17  | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 2  | 9  | 9  | 6  | 1  | -  | -  | -  | -  | -  | -  | -  | -  |   |
| UA9 = 18 | -       | 1  | 2  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 6  | 2  | 1  | -  | -  | -  | -  | -  | -  | 1  | -  | -  |   |
| UA0 = 19 | 8       | 6  | 2  | 1  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 3  | 8  | 9  |   |
| 4X = 20  | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 9  | 9  | 9  | 9  | 9+ | 9  | 6  | 6  | 2  | -  | -  | -  | -  |   |
| HZ = 21  | 2       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9  | 9  | 9  | 9  | 9  | 8  | 6  | 4  | 1  | 1  | 1  | 1  | 2  |   |
| VU = 22  | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 5  | 9+ | 9  | 7  | 2  | 1  | -  | -  | -  | 1  | 1  | 1  | -  |   |
| JT = 23  | 6       | 4  | 1  | 1  | -  | -  | -  | -  | -  | -  | -  | 2* | 4  | -  | -  | -  | 1  | -  | -  | -  | -  | -  | -  | 1  |   |
| VS6 = 24 | 5       | 2  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 5* | 6  | 4* | 2  | 2  | 1  | 1  | 1  | -  | -  | -  | -  | 1  | 7 |
| JA1 = 25 | 8       | 6  | 1  | -  | -  | -  | -  | -  | -  | -  | -  | 4* | 2* | 1* | -  | -  | -  | -  | -  | -  | 1  | 7  | 9+ | 9+ |   |
| HS = 26  | 5       | 2  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1* | 7  | 9+ | 9  | 8  | 6  | 4  | 4  | 4  | -  | -  | -  | -  |   |
| DU = 27  | 7       | 4  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 5* | 4* | 5  | 7  | 5  | 4  | 2  | -  | -  | -  | -  | 4  | 9  |   |
| YB = 28  | 5       | 1  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 3* | 2  | 9  | 9+ | 9  | 9  | 9  | 9+ | 7  | -  | -  | -  | 1  |   |
| VK6 = 29 | 8       | 2  | 1  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 9  | 9+ | 9  | 9  | 7  | -  | -  | -  | 8  | 9  |   |
| VK3 = 30 | 4       | 5  | 3  | 1  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9  | 7  | 2  | -  | -  | 1  | 7  | 6  | 5  | 5  | 5  |   |
| KH6 = 31 | 9       | 9  | 6  | 3  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9  | 9  | 9  | 9  | 9  | 9  | 9  | 9  |   |
| KH8 = 32 | 8       | 9  | 8  | 5  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 6  | -  | -  | 4  | 8  | 8  | 8  | 8  | 8  | 7  | 8  |   |
| CN = 33  | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 8  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 8  | 2  | -  | -  |   |
| SU = 34  | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 9  | 9  | 9  | 9  | 9+ | 9+ | 9  | 8  | 5  | 2  | -  | -  | -  |   |
| 6W = 35  | 1       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9  | 9+ | 9  | 9  | 9  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 8  |   |
| D2 = 36  | 8       | 1  | -  | 1  | 1  | 5  | -  | -  | -  | -  | 8  | 8  | 8  | 7  | 8  | 9  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9  |   |
| 5Z = 37  | 5       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 8  | 8  | 8  | 8  | 9  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9  | 8  |   |
| ES6 = 38 | 3       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 7  | 6  | 5  | 5  | 6  | 8  | 9  | 9  | 9+ | 9+ | 9+ | 9+ | 9  | 9  |   |
| FR = 39  | 4       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 6  | 6  | 6  | 7  | 8  | 9  | 9  | 9+ | 9+ | 9+ | 9+ | 9  | 8  | 8  |   |
| FJL = 40 | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 2  | 4  | 4  | 5  | 4  | 4  | 2  | -  | 1  | -  | -  |   |

Expected signal levels using 1500 W and 4-element Yagis at 60 feet at each station.



# Propagation Predictions

Scaling signal levels for different size stations:

- Subtract 2 S units for a dipole instead of a Yagi
- Subtract 3 S units for a dipole at 50' instead of a Yagi at 100'
- Subtract 1 S unit for a dipole at 50' rather than a dipole at 100'
- Subtract 3 S units for 100 W rather than 1500 W



# Propagation Predictions

15 Meters: Feb. 2003, YCCC, for SSN = High, Sigs in S-Units. By N6BV, ARRL.

| Zone     | UTC --> |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |    |
|----------|---------|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
|          | 00      | 01 | 02 | 03 | 04 | 05 | 06 | 07 | 08 | 09 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 |
| KL7 = 01 | 9       | 5  | 1  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 2  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ |
| VO2 = 02 | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 5  | 7  | 8  | 8  | 8  | 7  | 4  | 1  | 4  |
| W6 = 03  | 9+      | 9  | 2  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 5  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |
| W0 = 04  | 9+      | 9+ | 6  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |
| W3 = 05  | 1       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 1  | 1  | 1  | 1  | -  | -  | -  | -  | -  | -  | -  | 1  |
| XE1 = 06 | 9       | 5  | 9  | 7  | 1  | 1  | 1  | 2  | 5  | 4  | -  | -  | 8  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |
| TI = 07  | 9       | 4  | 9  | 7  | 5  | 3  | 2  | 3  | 4  | 2  | -  | 2  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |
| VP2 = 08 | 9+      | 9  | 7  | 4  | 4  | 4  | 4  | 4  | 1  | -  | 4  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |
| P4 = 09  | 9       | 9+ | 8  | 7  | 6  | 6  | 5  | 6  | 3  | -  | 1  | 4  | 8  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ |
| HC = 10  | 8       | 7  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 7  | 5  | 9+ | 9+ | 9+ | 9  | 9  | 9  | 9  | 9  | 9  | 9  | 4  |
| PY1 = 11 | 9       | 7  | 4  | 2  | 3  | 4  | 4  | 1  | -  | -  | 2  | 9  | 9+ | 9  | 8  | 7  | 8  | 8  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ |
| CE = 12  | 9+      | 8  | 5  | 4  | 3  | 3  | 2  | 2  | -  | -  | -  | 9  | 9  | 8  | 8  | 7  | 8  | 8  | 9  | 9  | 9  | 9  | 9  | 9  |
| LU = 13  | 9+      | 7  | 5  | 4  | 2  | 4  | 4  | 3  | -  | -  | 5  | 9+ | 9  | 8  | 7  | 7  | 8  | 8  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ |
| G = 14   | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 2  | -  | -  | -  |
| I = 15   | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 6  | 9+ | 9+ | 9+ | 9+ | 9+ | 8  | 9  | 2  | -  | -  | -  | -  |
| UA3 = 16 | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 6  | 9  | 9  | 9  | 8  | 5  | 1  | -  | -  | -  | -  | -  | -  |
| UN = 17  | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 2  | 9  | 9  | 6  | 1  | -  | -  | -  | -  | -  | -  | -  | -  |
| UA9 = 18 | -       | 1  | 2  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 6  | 2  | 1  | -  | -  | -  | -  | -  | -  | 1  | -  | -  |
| UA0 = 19 | 8       | 6  | 2  | 1  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 3  | 8  | 9  |    |
| 4X = 20  | -       | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 9  | 9  | 9  | 9  | 9+ | 9  | 6  | 6  | 2  | -  | -  | -  | -  | -  |
| HZ = 21  | 2       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9  | 9  | 9  | 9  | 9  | 8  | 6  | 4  | 1  | 1  | 1  | 1  | 2  |
| VU = 22  | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 5  | 9+ | 9  | 7  | 2  | 1  | -  | -  | 1  | 1  | 1  | 1  | -  |
| JT = 23  | 6       | 4  | 1  | 1  | -  | -  | -  | -  | -  | -  | -  | 2* | 4  | -  | -  | -  | 1  | -  | -  | -  | -  | -  | -  | 1  |
| VS6 = 24 | 5       | 2  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 5* | 6  | 4* | 2  | 2  | 1  | 1  | 1  | -  | -  | -  | 1  | 7  |
| JAL = 25 | 8       | 6  | 1  | -  | -  | -  | -  | -  | -  | -  | -  | 4* | 2* | 1* | -  | -  | -  | -  | -  | 1  | 7  | 9+ | 9+ | -  |
| HS = 26  | 5       | 2  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1* | 7  | 9+ | 9  | 8  | 6  | 4  | 4  | 4  | -  | -  | -  | -  |
| DU = 27  | 7       | 4  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 5* | 4* | 5  | 7  | 5  | 4  | 2  | -  | -  | -  | 4  | 9  | -  |
| YB = 28  | 5       | 1  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 3* | 2  | 9  | 9+ | 9  | 9  | 9  | 9+ | 7  | -  | -  | 1  | -  |
| VK6 = 29 | 8       | 2  | 1  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 9  | 9+ | 9  | 9  | 7  | -  | -  | 8  | 9  | -  |
| VK3 = 30 | 4       | 5  | 3  | 1  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9  | 7  | 2  | -  | -  | 1  | 7  | 6  | 5  | 5  | -  |
| KH6 = 31 | 9       | 9  | 6  | 3  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9  | 9  | 9  | 9  | 9  | 9  | 9  | 9  |
| KH8 = 32 | 8       | 9  | 8  | 5  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 6  | -  | -  | 4  | 8  | 8  | 8  | 8  | 7  | 8  | -  |
| CN = 33  | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 8  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 8  | 2  | -  | -  | -  |
| SU = 34  | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 9  | 9  | 9  | 9  | 9+ | 9+ | 9  | 8  | 5  | 2  | -  | -  | -  |
| 6W = 35  | 1       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 9  | 9+ | 9  | 9  | 9  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 8  |
| D2 = 36  | 8       | 1  | -  | 1  | 1  | 5  | -  | -  | -  | -  | 8  | 8  | 8  | 7  | 8  | 9  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9  |
| 5Z = 37  | 5       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 8  | 8  | 8  | 8  | 9  | 9  | 9+ | 9+ | 9+ | 9+ | 9+ | 9+ | 9  | 8  |
| ES6 = 38 | 3       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 7  | 6  | 5  | 5  | 6  | 8  | 9  | 9  | 9+ | 9+ | 9+ | 9+ | 9  | 9  |
| FR = 39  | 4       | -  | -  | -  | -  | -  | -  | -  | -  | -  | 6  | 6  | 6  | 7  | 8  | 9  | 9  | 9+ | 9+ | 9+ | 9+ | 9  | 8  | -  |
| FJL = 40 | -       | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | -  | 1  | 2  | 4  | 4  | 5  | 4  | 4  | 2  | -  | 1  | -  | -  |

Expected signal levels using 1500 W and 4-element Yagis at 60 feet at each station.





# Propagation Predictions

**For example: W1 to Zone 22, VU2**

On 15 meters, VU2 uses 100 W to a 50' high dipole instead of 1500 W to 100' high 4-ele. Yagi.

At 14 UTC, base prediction is for S9 signal.  
Signal = S9 - 3 (50' dipole) - 3 (100 W) = S3

At 15 UTC, base prediction is for S7 signal.  
Signal = S7 - 3 (50' dipole) - 3 (100 W) = S1



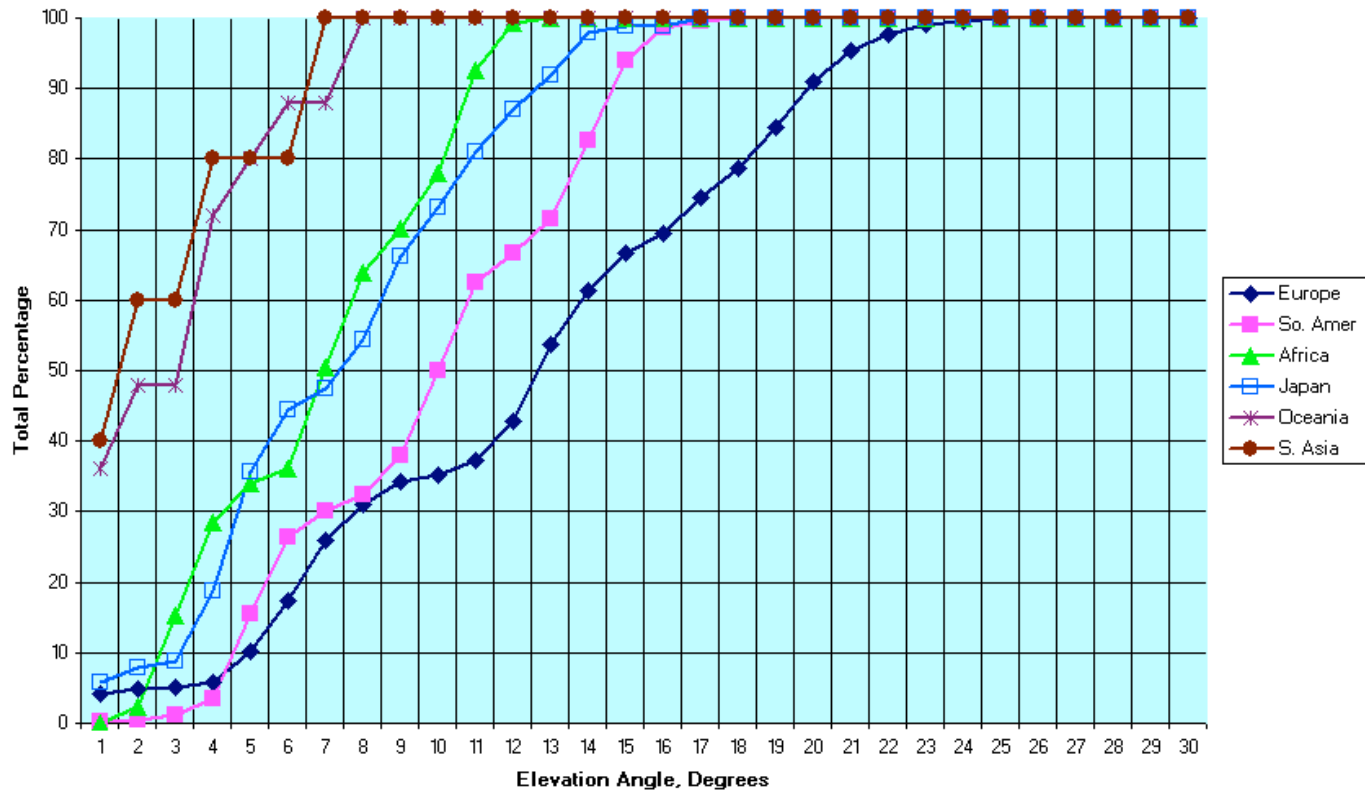
# The Importance of Low Angles for DX

- And just in case you didn't know it, low takeoff angles are very important for DX work!
- Even on the low bands.



# The Importance of Low Angles for DX, 80 Meters

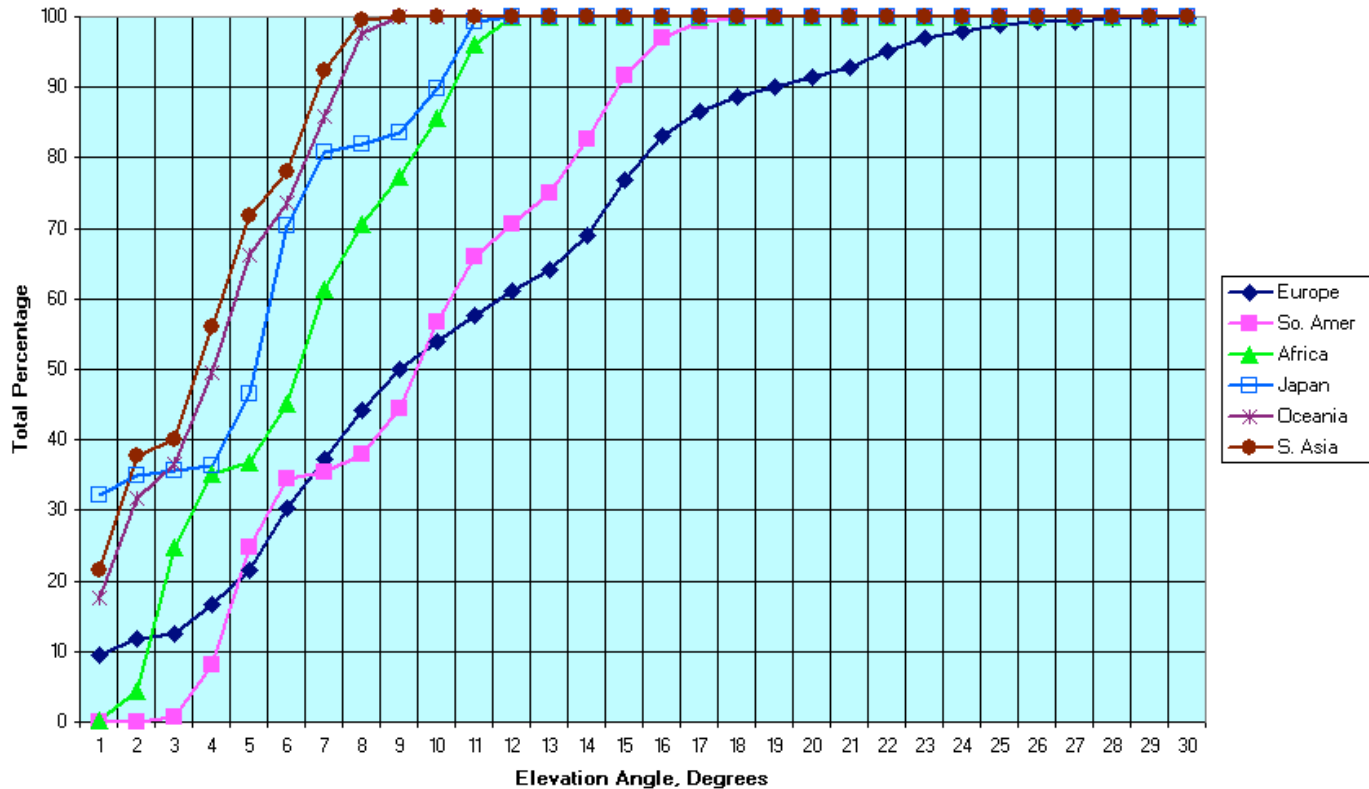
Percentage of Time 80 Meters is Open, At or Below Each Elevation Angle  
Boston to World





# The Importance of Low Angles for DX, 40 Meters

Percentage of Time 40 Meters is Open, At or Below Each Elevation Angle  
Boston to World



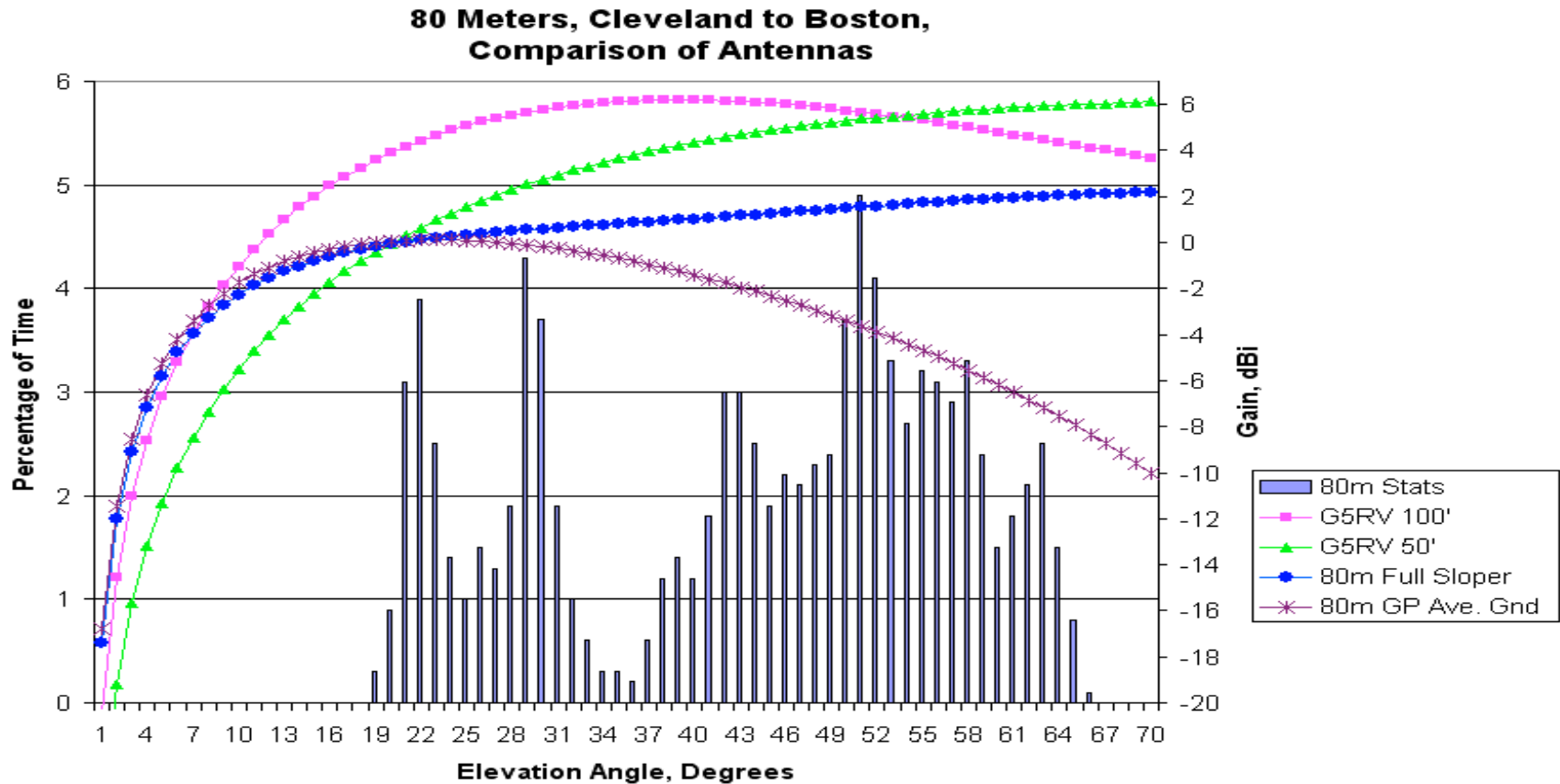


# Domestic QSOs

What about short-range communications on 80 and 40 meters -- say, for the ARRL Sweepstakes or for Field Day?



# Higher Angles for 80-Meter Domestic Work

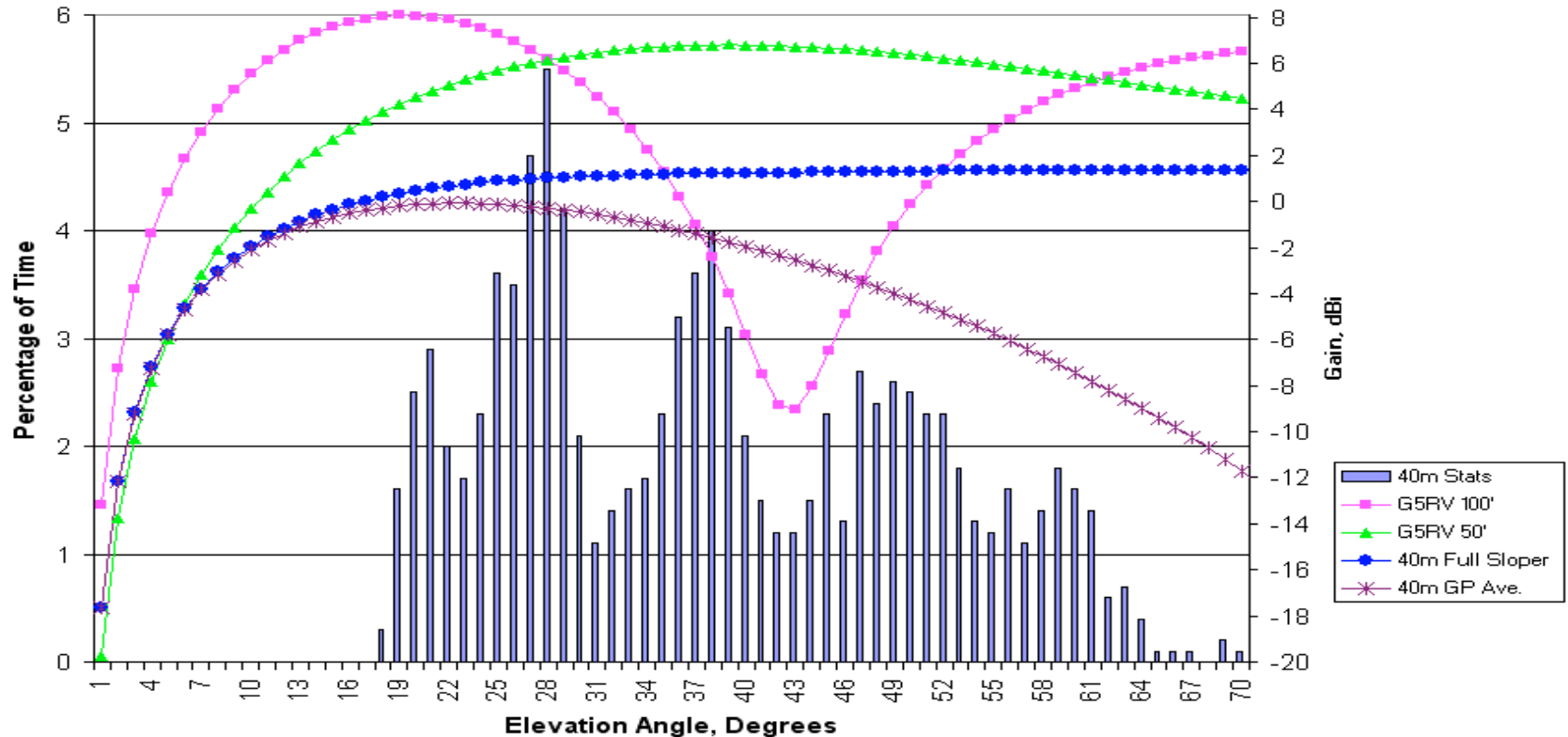


A 100' 80-m Dipole is excellent for Field Day



# Higher Angles for 40-Meter Domestic Work

40 Meters, Cleveland to Boston,  
Comparison of Antennas



A 50' 40-m Dipole is a Killer for Field Day!



# A Takeoff-Angle Quiz

A station in London has a 22-foot high, 15-meter dipole in his garden. (This puts his antenna about a halfwave above ground.)

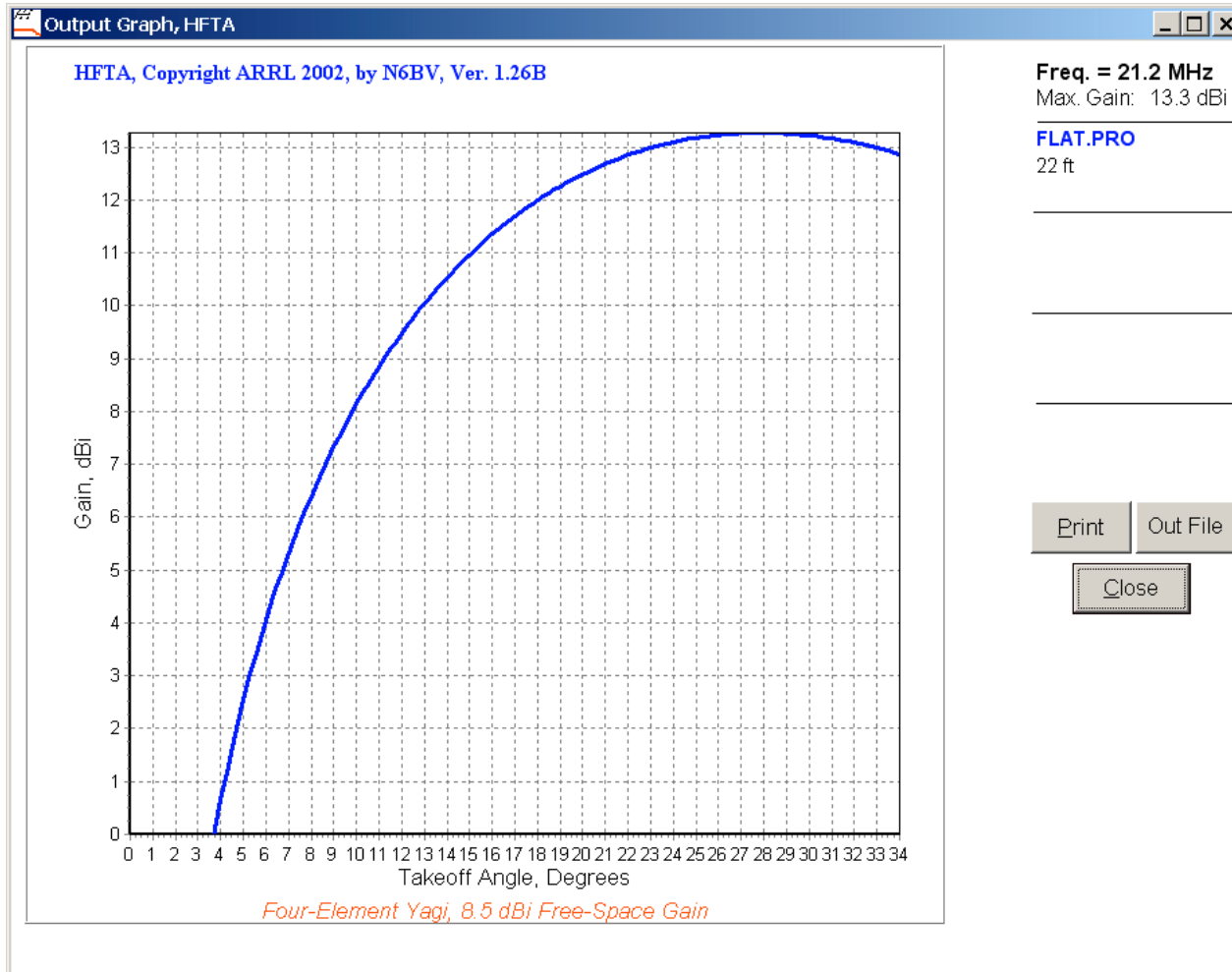
What is the takeoff angle?

- a.  $5^\circ$
- b.  $10^\circ$
- c.  $15^\circ$
- d.  $30^\circ$





# A Takeoff-Angle Quiz



30° = TOA for  
a halfwave  
over flat  
ground



# A Propagation Quiz

A station in London is running 100 W to a halfwave high, 15-meter dipole in his garden. What mode & elevation angle to Boston is he using at 16 UTC in February, during a high part of the solar cycle?

- a. 2F2 mode at  $5^\circ$
- b. 3F2 mode at  $15^\circ$
- c. 4F2 mode at  $28^\circ$



# The Ionosphere Controls

Scrollw:C:\ITSHFBC\RUN\VOACAPx.out 94015 bytes

File Edit

SUMMARY 4 MODES FREQ = 21.2 MHZ UT = 16.0

|            | 2.F2    | 3.F2    | 3.F2              | 3. E    | Most REL |
|------------|---------|---------|-------------------|---------|----------|
| TIME DEL.  | 18.19   | 18.94   | 19.47             | 17.88   | 18.19    |
| ANGLE      | 4.86    | 14.68   | 18.16             | 4.10    | 4.86     |
| VIR. HITE  | 256.09  | 302.93  | 366.86            | 125.30  | 256.09   |
| TRAN. LOSS | 142.19  | 143.34  | 155.72            | 970.06  | 142.19   |
| T. GAIN    | 2.24    | 10.84   | 12.05             | 0.88    | 2.24     |
| R. GAIN    | 10.00   | 10.00   | 10.00             | 10.00   | 10.00    |
| ABSORB     | 4.88    | 3.10    | 2.68              | 5.01    |          |
| FS. LOSS   | 133.71  | 134.06  | 134.30            | 133.56  |          |
| FIELD ST.  | 1.53    | 0.38    | -12.00            | -826.33 | 4.11     |
| SIG. POW.  | -122.19 | -123.34 | -135.72           | -950.06 | -119.61  |
| SNR        | 57.19   | 56.04   | 43.66             | -770.67 | 59.77    |
| MODE PROB  | 0.93    | 0.44    | 0.44              | 0.00    | 0.93     |
| R. PWRG    | 1000.00 | 1000.00 | 1000.00           | 1000.00 | -16.77   |
| RELIABIL   | 0.86    | 0.74    | 0.51              | 0.00    | 0.87     |
| SERU PROB  | 1.00    | 1.00    | 0.56              | 0.00    | 1.00     |
| SIG LOW    | 15.70   | 25.00   | 25.00             | 10.74   | 17.89    |
| SIG UP     | 6.46    | 13.58   | 22.24             | 6.14    | 12.09    |
| NOISE =    | -179    |         | S. POWER = -119.6 |         |          |
| SIGNAL =   | 10.7    | 9.5     | 6.1               | / 4.5   | 3.6 1.3  |
| NOISE =    | 6.1     | -179.4  | 2.3               | / 2.1   | 2.1 1.6  |
| RELIAB =   | 12.3    | 59.8    | 18.9              |         |          |
| SPROB =    | 4.6     | 57.2    | 4.6               |         |          |

CCIR Coefficients METHOD 25 VOACAP 02.1106W PAGE 32

22'  
Dipole  
gain

Strongest  
Mode,  
weak as it  
is



# The Ionosphere is Boss!

“You should always remember that it is the *ionosphere* that controls the elevation angles, *not* the transmitting antenna. The elevation response of a particular antenna only determines how strong or weak a signal is, at whatever angle (or angles) the ionosphere is supporting at that particular instant, for that propagation path and for that frequency.”

This is on page 23-25, in *The ARRL Antenna Book*,  
19th Edition.



# Some Useful Propagation URLs

## **160-meter propagation information:**

<http://solar.spacew.com/www/160pred.html>

## **Planetary kp indices:**

[http://www.sel.noaa.gov/ftpmenu/plots/2002\\_plots/kp.html](http://www.sel.noaa.gov/ftpmenu/plots/2002_plots/kp.html)

## **General propagation information:**

<http://dx.qsl.net/propagation/index.html>

## **Solar cycle information:**

<http://www.sec.noaa.gov/SolarCycle/>

## **Effective sunspot number:**

<http://www.nwra-az.com/spawx/ssne24.html>

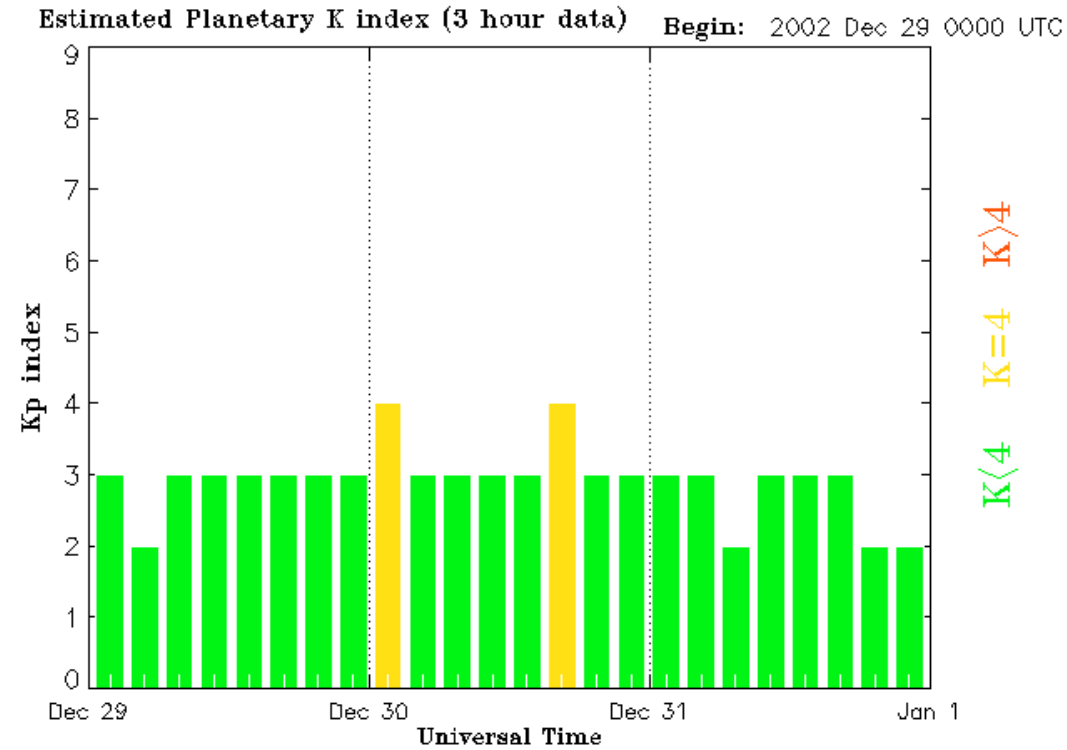




# Some Useful Propagation URLs

## Planetary kp indices:

[http://www.sel.noaa.gov/ftpmenu/plots/2002\\_plots/kp.html](http://www.sel.noaa.gov/ftpmenu/plots/2002_plots/kp.html)



Updated 2003 Jan 1 02:45:03 UTC

NOAA/SEC Boulder, CO USA



# Some Useful Propagation URLs

**Solar cycle information:**

<http://www.sec.noaa.gov/SolarCycle/>

